

Extraction Behavior of Sr(II) from Nitric Acid Solution using DtBuCH18C6 Containing Ionic Liquid Extraction System and its medical application

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4',4'(5")-di-(*tert*-butyl cyclohexano)-18-crown-6 (DtBuCH18C6) as an extractant in combination with three types of ionic liquids, $[C_4mim][X]$ (X = NfO, NTf₂, FAP) as solvents to separate Sr(II) effectively from HNO₃ solution. Under the experimental conditions, within the acidity range studied, the D_{Sr} follows the order of $[C_4mim][NfO] > [C_4mim][NTf_2] > [C_4mim][FAP]$. In their extraction systems, D_{Sr} decreases with increasing concentration of HNO₃ solution. Thermodynamic parameters for the extraction of Sr(II) tested elements were calculated using the Van't Hoff equation, showing that the reaction is spontaneous and exothermic. Existence of inorganic salts such as KNO₃ usually reduces E_{Sr} for all systems, and the decreasing degree is much larger than that of NaNO₃. The extraction systems exhibited high extraction efficiency and high selectivity for Sr(II) from simulated HLLW containing 20 typical elements and 2M HNO₃. From the results, the present system may provide an alternative for extraction of Sr(II) under HLLW conditions.

1. Introduction

In order to minimize the long-term radiological risk and reuse of valuable nuclides in the field of spent nuclear fuel reprocessing, the partitioning of ⁹⁰Sr and of some specific fission products (FPs) from high-level liquid waste (HLLW) is very desirable [1-3]. The heat-generated elements, ⁹⁰Sr, having a half-life of 28 years and contributes about 25% of heat generation in HLLW(~1.1 kg/1 tHU, 45 GWd/t) [4] with its daughter nuclide ⁹⁰Y. Furthermore, ⁹⁰Y is also expected for the utilization as radioactive material in the medicine field. Therefore the selective separation of ⁹⁰Sr from HLLW is necessary. A number of recovery methods have been reported in literature for the separation of Sr(II) from HLLW, such as ion exchange [5–9], solvent extraction [10–14] and extraction chromatography [15-16]. Over the last decade, in the ionic liquids extraction has selective extractability to Sr(II) that has been widely used for extraction process. Ionic liquids are composed of heterocyclic organic cations and inorganic anions and have even more advantageous properties, such as nonvolatility, nonflammability, thermal and electrochemical stabilities and conductivity instead of the traditional diluents, enhancement of extraction efficiency, possibly leading to cost-reduction in extraction processes. This evaluation study was carried out based on a novel extraction process for HLLW treatment which was proposed by our group [17]. In this extraction process, the FPs elements PGMs and Cs(I) have been separated from simulated HLLW firstly by [C₄min][NfO] and Calix[4]arene-R14 as an extractant and 1-alkyl-3-methylimdazolium bis(trifluoromethylsulfonyl)amide ($[C_n mim][NTf_2]$) solvents as



successfully.

In this work, the extraction of Sr(II) from HNO_3 solution has been investigated using DtBuCH18C6 as an extractant in combination with three kinds of ionic liquid $[C_4mim][X]$ (X = NfO, NTf₂, FAP) as solvents, where DtBuCH18C6 is 4,4',(5')-di-(*tert*-butyl cyclohexano)-18-crown-6, $[C_4mim]^+$ is 1-butyl-3-methylimidazolium and $[NfO]^-$ is nonafluorobutane-sulfonate, $[NTf_2]^-$ is bis(trifluoro-methyl sulfonyl)amide, $[FAP]^-$ is tris(pentafluoroethyl)trifluorophosphate. The extraction system was studied in detail with regard to different extraction parameters such as the concentration of HNO₃, concentration of extractant, temperature, concentration of inorganic salts, and under coexistence of various metals, on the extraction of Sr(II).

2. Experimental

2.1 Materials

4',4'(5")-di(*tert*-butylcyclohexano)-18-crown-6 (DtBuCH18C6, 90 wt%) was purchased from Sigma-Aldrich Chemical Co. and used without purification. The ionic liquid of $[C_4mim][NfO]$ was synthesized. Its synthesis method was reported in detail by Kozonoi [18]. $[C_4mim][NfC]$, $[C_4mim][FAP]$ ionic liquids were purchased from Sigma-Aldrich Chemical Co. The molecular structure of DtBuCH18C6 and $[C_4mim][X]$ (X = NTf₂, NfO, FAP) are shown in Figure 1. Chemical reagents, NaNO₃, KNO₃, AgNO₃, Sr(NO₃)₂, Ba(NO₃)₂, RE(NO₃)₃·6H₂O (RE = Y, La, Ce, Pr, Nd, Sm, and Gd), ZrO(NO₃)₂·2H₂O, (NH₄)₆Mo₇O₂₄·4H₂O, Cr(NO₃)₃, Mn(NO₃)₂·6H₂O, Fe(NO₃)₃·9H₂O, Ni(NO₃)₂·6H₂O, and Zn(NO₃)₂·6H₂O were of analytical grade and supplied by Kanto Chemical Co.



Figure 1. Chemical structure of the cations $[C_4min]^+$ and anions $[NfO]^-$, $[NTf_2]^-$, $[FAP]^-$ and extractant (DtBuCH18C6).

2.2 Batch extraction method

The extraction behaviors of metal ions for DtBuCH18C6 containing ionic liquid extraction system were estimated by batch methods. An aqueous solution (2 cm^3) containing 5 mM Sr(II) ion was contacted with 2 cm³ of ionic liquid containing DtBuCH18C6 in a thermostatic bath up to 15 min, which was found to be sufficient for attaining equilibrium. The concentrations of metal ions were



measured using an atomic absorption spectrophotometer (AAS) and inductively coupled plasma atomic emission spectrometer (ICP-AES). The distribution ratios (D_{Sr}) and extraction efficiencies (E_{Sr}) were calculated as follows:

$$D_{\rm Sr} = \frac{C_{\rm IL}}{C_{\rm Aq}} = \frac{C_{0,\rm Aq} \times \frac{V_{0,\rm Aq}}{V_{\rm IL}} - C_{\rm Aq} \times \frac{V_{\rm Aq}}{V_{\rm IL}}}{C_{\rm Aq}} \tag{1}$$

where $C_{0,Aq}$ and C_{Aq} represent the initial and final concentrations of Sr(II) in an aqueous solution, $V_{0,Aq}$ and V_{Aq} (cm³) indicate the volume of the aqueous phase before and after extraction, respectively, and V_{IL} (cm³) is the volume of the ionic liquid phase after extraction.

3. Results and Discussion

3.1 Extraction kinetics in ILs

In order to evaluate the equilibrium time of Sr(II) for DtBuCH18C6 containing ILs extraction systems, the effect of mixing time on E_{Sr} was examined in the presence of 2 M HNO₃ by the batch method. The E_{Sr} increases with an increase in mixing time and reaches an equilibrium state within 10 min. Under the experimental conditions, the E_{Sr} shows an order of [C₄mim][NfO] > [C₄mim][NTf₂] > [C₄mim][FAP]. The data showed that the extraction capability of Sr(II) decreased with anions under same conditions. This result shows that the extraction capabilities for metal ions have a strong preference for the aqueous phase.

3.2 Effects of HNO₃ solution concentration

To understand the effect of HNO₃ concentration, the extraction behavior of 5 mM Sr(II) into DtBuCH18C6 (10 mM) containing ILs systems were examined at different concentrations of HNO₃ from 0.015 M to 4 M by batch method (Figure 2). As for Sr(II)), a decrease in the D_{Sr} for the [C₄mim][NfO], [C₄mim][NTf₂] systems with increasing concentrations of HNO₃ is observed. In

contrast, $[C_4mim][FAP]$ was considerably low in the all range of HNO₃ concentration. Within the acidity range studied, the D_{Sr} values for Sr(II) maintain the order of $[C_4mim][NfO] >$ $[C_4mim][NTf_2] > [C_4mim][FAP].$

The extraction mechanism with participation of hydrophobic ILs has been continuously studied. Similar results were observed in a study conducted by Luo et al. [19]. Luo has reported that the hydrophobicity of the IL anion has controlling extraction strength. Moreover, several studies have reported that the extraction ratio decreases with an increase in the HNO₃ concentration. Xu et al. has shown that the competition of H^+ might be a leading factor that



Figure 2. Dependence of $D_{\rm Sr}$ on HNO₃ concentration.



causes an overall decrease in the extraction efficiency [20]. In the same manner, it is possible that competition of H^+ accounts for the decrease in D_{Sr} with an increase in the HNO₃ concentration. These observations suggest that one of the mechanisms for extraction is cation exchange.

3.3 Influence of the DtBuCH18C6 concentration

To understand the extractant effect, the extraction behavior of Sr(II) into DtBuCH18C6 containing ILs systems in a 2 M HNO₃ solution was investigated at different concentrations. Figure 3 shows the relation between E_{Sr} and DtBuCH18C6 concentration in combination with [C₄mim][X]. As

shown in Figure 3, $E_{\rm Sr}$ increases with increasing DtBuCH18C6 concentration. The [C₄mim][NTf₂] and [C₄mim][FAP] showed no extraction of Sr(II) in the absence of DtBuCH18C6, i.e., ILs themselves cannot extract Sr(II) in the absence of extractants. On the other hand, proper [C₄mim][NfO] has extraction ability for Sr(II). Kozonoi et al. has shown that [C₄mim][NfO] extract various metal ionic species from the aqueous solution. This observation suggests that [NfO] anion is extractant for Sr(II) in [C₄mim][NfO]. The results in Figure 3 also indicate that the extraction capability of the three selected [C₄mim][X] systems follows the general order of $[C_4 mim][NfO] > [C_4 mim][NTf_2] >$



Figure 3. Dependence of D_{Sr} on DtBuCH18C6 concentration.

 $[C_4mim][FAP]$ under given conditions. The $[C_4mim][NfO]$ matches best with DtBuCH18C6 to extract Sr(II).

A linear regression analysis of the D_{Sr} resulted in a straight line with a slope of 1.1, suggesting the involvement of 1 molecule of DtBuCH18C6 during the extraction processes as shown in Eq(3) and (4).

Such a phenomenon has been observed by Dietz and Stepinski while studying the extraction of sodium by crown ether (dicyclohexano-18-crown-6) under low acid conditions [21].

$$Sr^{2+} + DtBuCH18C6 + \overline{2C_4mim^+} \Leftrightarrow \overline{\left[(Sr \cdot DtBuCH18C6\right]^{2+}} + 2C_4mim^+$$
(3)

$$Sr^{2+} + 2NO_3^- + \overline{DtBuCH18C6} \Leftrightarrow \overline{[(Sr(NO_3) \cdot DtBuCH18C6]]}$$
(4)

3.4 Extraction thermodynamics

To understand the temperature effect, the extraction behavior of Sr(II) onto DtBuCH18C6 containing ILs systems in 2 M HNO₃ solution was investigated at different temperatures. In order to gain insight into the thermodynamic nature of the extraction process, several thermodynamic parameters for the present system were calculated. The Gibbs free energy, ΔG° , is the fundamental



criterion of spontaneity. Reactions occur spontaneously at a given temperature if ΔG° is a negative quantity. The Gibbs free energy of the extraction process is given by the equation as follows

$$\Delta G^{\circ} = -RT \times \ln D \tag{5}$$

Otherwise, the values of enthalpy change(ΔH°) and entropy change (ΔS°) for Sr(II) in the extraction processes can be calculated from the slope and intercept of the plots of ln*D vs*. 1/*T* by the van't Hoff equation as follows

$$\ln D = \frac{-\Delta H^{\circ}}{R \cdot T} + \frac{\Delta S^{\circ}}{R} \tag{6}$$

where *R* is the gas constant (8.314 J mol⁻¹ K⁻¹), *T* is the absolute temperature in Kelvin, is the distribution ratios (D_{Sr}) on equilibrium state defined as Eq. (1).

The experimental temperature was controlled in the range of 288 to 323 K and the corresponding plots of $\ln D vs. 1/T$ are depicted in Figure 4. From the plots in Figure 4, all the calculated parameters of the extraction reactions for DtBuCH18C6 containing ILs systems, ΔG° , ΔH° , and ΔS° are summarized in Table 1. The negative value of ΔG° means the extraction processes occur spontaneously at a given temperature. The change in ΔH° for Sr(II) is charged to be parative, confirming the evolution



Figure 4. Van't Hoff plots for the extraction of Sr(II) on DtBuCH18C6/ ILs. [HNO₃] = 2.0 M, [DtBuCH18C6] = 10 mM, [Sr] = 5 mM

observed to be negative, confirming the exothermic nature of the extraction processes.

Tem	$\Delta G^{\circ} (\text{kJ mol}^{-1})$			ΔI	$\Delta H^{\circ} (\text{kJ mol}^{-1})$			$\Delta S^{\circ} (\text{kJ mol}^{-1} \text{K}^{-1})$		
(K)	[NfO]	[NTf ₂]	[FAP]	[NfO]	[NTf ₂]	[FAP]		[NfO]	[NTf ₂]	[FAP]
288	-2.59	-0.27	6.81							
293	-	-0.04	7.17	-11.15	-13.46	-13.77		-0.030	-0.046	-0.071
298	-2.30	0.19	-							
303	-	0.42	7.89							
308	-2.00	-	-							
323	-1.55	1.33	9.32							

Table 1. Values of the thermodynamic parameters for extraction of Sr(II) on DtBuCH18C6/ILs

3.5 Effect of inorganic salts

HLLW containing a large quantity of inorganic salts derived from alkaline liquid waste has an especially large amount of Na(I). To examine the applicability of separation process for HLLW, it is necessary to study the effects of NaNO₃ and KNO₃ on the extraction of Sr(II) using DtBuCH18C6 containing ILs systems.





Figure 5. Dependence of the extraction efficiency of Sr(II) in DtBuCH18C6/ILs on the concentration of inorganic salts. ([HNO₃] = 2.0 M, [DtBuCH18C6] = 10 mM, [Sr] = 5 mM, T=295K)

As shown in Figure 5, the addition of the two salts will generally reduce the extraction efficiency of Sr(II); however, the E_{Sr} of solutions containing Na(I) was much larger than that of K(I). This can be explained by the similar ionic radius between K(I) and Sr(II), which causes much more competition with the crown ether complex.

3.6 Separation of Sr(II) for simulated HLLW

The components in HLLW after removing actinides are very complicated. Apart from the 90 Sr radioactive nuclide, there are many other coexisting elements such as Cs, Ba, PGMs, rare earths and minor actinide. To understand the separation behavior of Sr(II) as well as other fission products, a group partitioning experiment for a simulated HLLW containing 20 elements and 2 M HNO₃ was performed using the DtBuCH18C6 containing ILs systems at 298 K. The relevant extraction of Sr(II) is illustrated in Figure 6. All extraction systems exhibited a high distribution ratio and high selectivity for separation of Sr(II) and Ba(II) from sHLLW. The separation factor (SF) of Sr from most other elements such as Cs and PGMs is much higher. In addition, the SF of Y(III) is more than 10^3 . The results indicate that DtBuCH18C6 containing ILs systems show stronger extraction ability and selectivity for Sr(II) in the HLLW medium.



Figure 6. Extraction of Sr(II), Ba(II) from a sHLLW using DtBuCH18C6/ ILs. ($[H^+] = 2.0$ M, [DtBuCH18C6] = 100 mM, T=298 K)



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4. Conclusion

Extraction of Sr(II) ions using DtBuCH18C6 and three ILs as solvents has been investigated. All extraction systems are rapid reactions that reach extraction equilibrium in approximately 10 min. The extractions exhibit a decrease in D_{Sr} with increasing concentration of HNO₃. Within the HNO₃ concentration range studied, the D_{Sr} maintains the order of $[C_4mim][NfO] > [C_4mim][NTf_2] > [C_4mim][FAP]$. The calculated thermodynamic parameters of the extraction of Sr(II) based on Van't Hoff equation indicate that the reaction is spontaneous and exothermic. The existence of inorganic salts such as KNO₃ reduces the E_{Sr} for the three systems, and the degree of decrease is much larger than that of NaNO₃; however, the E_{Sr} of solution containing Na(I) was much larger than that of K(I). In the present system, a medium acidity extraction behavior has been revealed, which may provide an alternative method for extraction of Sr(II). This method was observed to effectively separate Sr(II) from the simulated HLLW, avoiding the use of high concentration of HNO₃ when using conventional solvents.

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